# HVAC LOAD CALCULATIONS AND THE ENERGY RATER

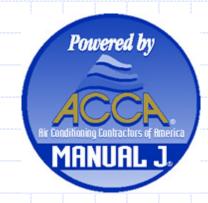


RESNET 2009

**Dennis J Stroer** 

**CALCS-PLUS** 

Venice Florida





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Research Toward Zero Energy Homes

#### **Accu-Size Heating & Cooling Ho**

Single glass

Double glass \_ SQUARE FOOTAGE ( Single glass patio \_ Double glass patio . Wood (no storm do Wood (w/storm doc Insulated metal doo SQUARE FOOTAGE ( Frame (no insulation Frame (3.5" insulation Frame (6" insulation Masonry (no insulat Masonry (1" insulat SQUARE FOOTAGE C No insulation \_\_\_ R-11 (3" insulation) R-19 (6" insulation) R-30 (10" insulation) SQUARE FOOTAGE C No insulation Carpet (no insulatio R-11 (3"+ insulation) SQUARE FOOTAGE C No insulation \_ Carpet or insulation PERIMETER OF SLAE Slab (no insulation) Slab (edge insulation)

SQUARE FOOTAGE OF WINDOWS			HEAT GAIN
North (single)	X 26	-	IILAI GAIN
North (double)			
NE & NW (single)			
NE & NW (double)			
East & West (single)			
East & West (double)		_	
		_	
SE & SW (single)			
SE & SW (double)			
South (single)		=	
South (double)	_ X 25	=	
SQUARE FOOTAGE OF DOORS			HEAT GAIN
Wood (no storm door)		=	
Wood (w/storm door)	_ X 9	=	
Insulated metal door	_ X 6	=	
SQUARE FOOTAGE OF NET WALLS			HEAT GAIN
Wall perimeter X _height		less	
glass and door area = net	wall		
No insulation		=	
R-13 (3.5" insulation)	_X3	=	
R-19 (6" insulation)	_ X 2	=	
SQUARE FOOTAGE OF CEILING			HEAT GAI
No insulation	X 22	=	
R-11 (3" insulation)	X 4.1	=	
R-19 (6" insulation)	X 2.6	=	
R-30 (10" insulation)	X 1.6	=	
SQUARE FOOTAGE OF FLOOR			HEAT GAIL
No insulation	Х3	-	
Carpet (no insulation)		=	
R-11 (3"+ insulation)		=	
Floor on slab		=	0
	_ 11 0		
INFILTRATION / VENTILATION  Home square feet	Y 3 5	_	HEAT GAIN
	_ A J.J		
INTERNAL GAINS			HEAT GAIN
Number of people X 530 =	-		1050
Kitchen & bath allowance			1250
Subtotal BTU/h heat gain		=	
GAINS FROM DUCTWORK			HEAT GAI
In crawl space - (subtotal BTU/h X .0	09)		
In attic - (subtotal BTU/h X .13)			

## Heating load (h

#### Cooling load (heat gain) - 95 degree day

SQUARE FOOTAGE OF WINDOWS			HEAT (
North (single)	X 26	=	William William
North (double)	X 21	=	3 <del>.</del>
NE & NW (single)	X 45	=	S
NE & NW (double)	X 35	=	a <del></del>
East & West (single)	X 60	=	-
East & West (double)	X 49	=	3 <del></del>
SE & SW (single)	X 50	=	-
SE & SW (double)	X 40	=	-
South (single)	X 36	=	
South (double)	X 25	=	
X 57 = X 22 =			

# INFILTRATION / VENTILATION Home square feet \_\_\_\_\_ X 4.9 = \_\_\_\_ OR Subtotal BTU/h heat loss = \_\_\_\_\_ LOSSES FROM DUCTWORK HE STA

=

OR, Just do the old stand-by!

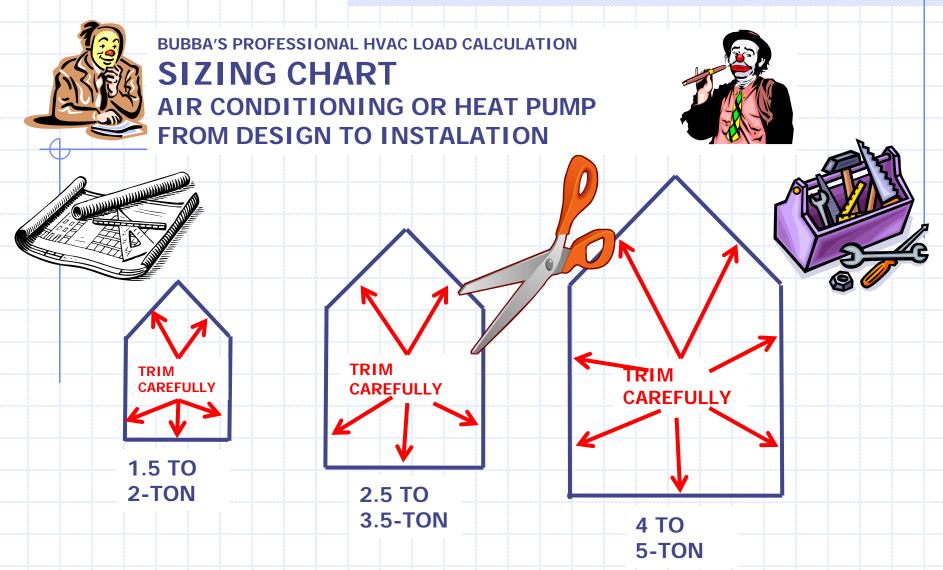
Total BTU/h heat loss = 80% furnace efficiency loss X .25 =

X SQ FT PER TON

Total BTU/h input needed

90% furnace efficiency loss X .12 =

In crawl space - (subtotal BTU/h X .10) In attic - (subtotal BTU/h X .08)



TRIM OUT VERY CAREFULLY ON DASHGED LINES, THEN FOLLOW INSTRUCTIONS BELOW

Stand on curb across from the home you are performing the calculation on. Look through the sizing holes locating the best match. For larger homes and or zoning use multiple Sizing Holes.

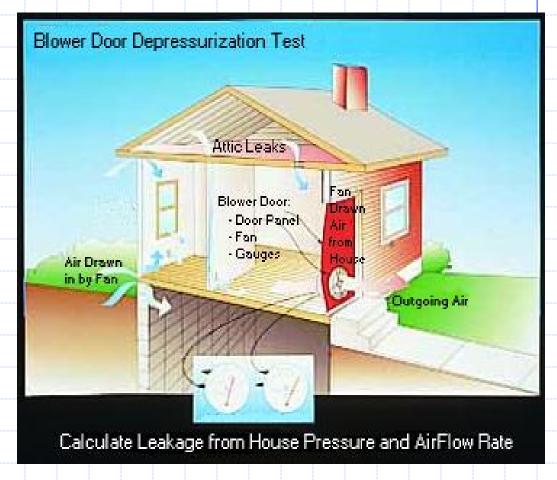
#### **HVAC Load Calculations.**

- Why should an Energy Rater perform HVAC Load Calculations?
- What is meant by a Room x Room calculation?
- Why use ACCA Manual J Version 8?
- MJ8 Sensitivities.
- How can an Energy Rater benefit?

# **Energy Raters and Air Flow**

Energy raters are already familiar with airflow. We use air flow as a tool to do energy ratings.





# Two types of Airflow.

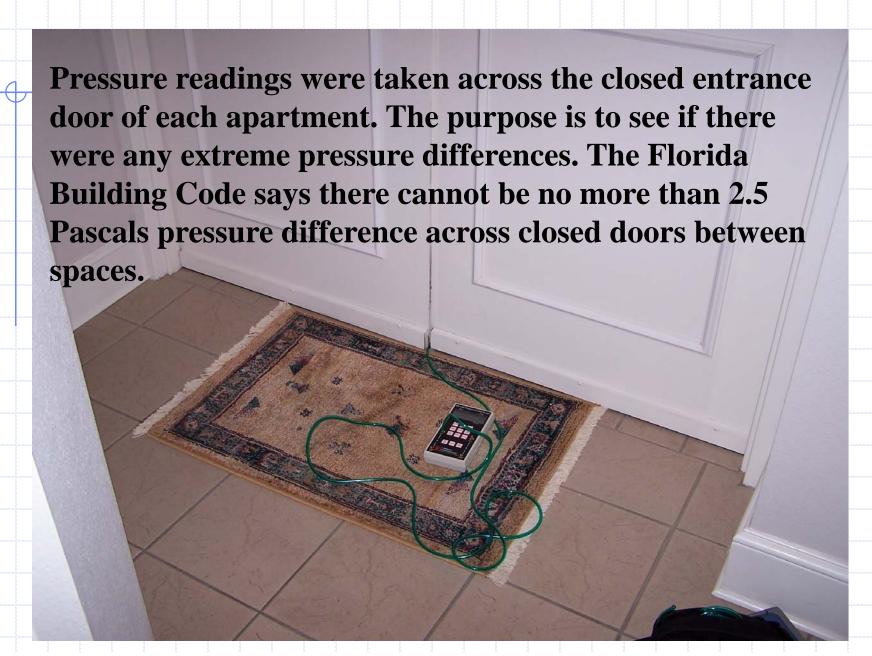
With respect to residential and commercial construction there are two kinds of airflow.

**Controlled and Uncontrolled** 



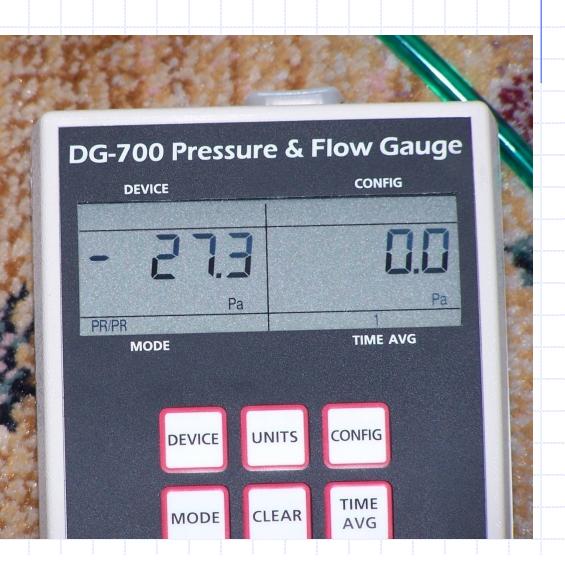
Energy Raters use controlled airflow to estimate the amount of uncontrolled airflow.

## **Uncontrolled Airflow**



#### **Uncontrolled Airflow**

The elevator lobby was found to be a - 27.3 Pascals with respect to the apartments. This means air in the elevator lobby is trying to go into the apartment.

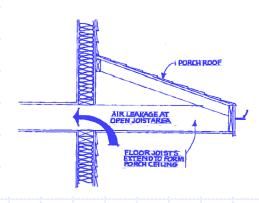


## **Uncontrolled Airflow**

Leaky buildings

Leaky Duct Systems

Unbalanced building pressures.





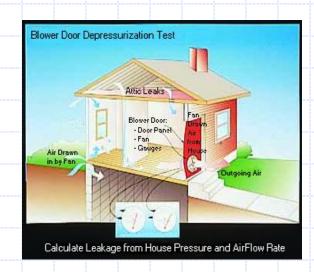


# Uncontrolled Airflow = Infiltration

Infiltration influences how the building reacts in terms of health, safety, durability, comfort, and energy efficiency.

- •Can be estimated with a high degree of accuracy.
- •Can be tested with a high degree of accuracy.
- •Can be eliminated or controlled.





# Duct Leakage

Influences how the building reacts in terms of health, safety, durability, comfort, and energy efficiency.

- •Can be estimated with a high degree of accuracy.
- •Can be tested with a high degree of accuracy.
- •Can be eliminated.







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# As <u>Energy Raters</u> we understand uncontrolled airflow.

# So lets talk about controlled airflow.

### **Controlled Airflow**

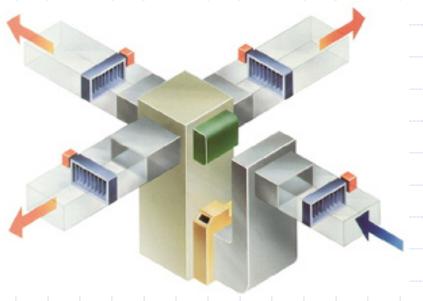
**Open and closing windows** 

Table fan

Air conditioning systems.







# The Building is a System

Air Conditioning is a Sub System

Air Conditioning Conditions Air, duh!

**Air Conditioning Moves Air** 

**Air Conditioning Blows and Sucks** 

Air Conditioning Affects Building Pressure

Air Conditioning Makes the Building Come Alive

### Room Airflow

#### Relating to Air Conditioning Systems

Determined by the estimated Heat Gain/Loss; Cooling or heating which ever has been chosen to dominate the system design.

**HVAC** Load calculations should be performed on a Room x Room basis.

Based on the Heat Loss/Gain through the building envelope and internal gains relative to each room.

#### Room x Room Loads

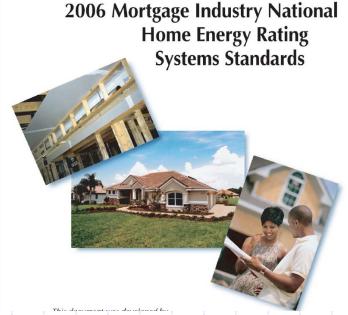
- If the HVAC system is the backbone of the house as a system. The HVAC load calculation is the backbone of the HVAC system
- Required to determine supply CFM for each room
- Required to select Supply Outlets
- Required to select Return Inlets
- Required to design a Duct System
- Required to diagnose comfort problems

303.5.1.5 Manufacturer's Equipment Performance Ratings (e.g., HSPF, SEER, AFUE) shall be corrected for local climate conditions and mis-sizing of equipment. To determine equipment mis-sizing, the capacity of heating and cooling vapor compression equipment shall be calculated in accordance with ACCA Manual J,

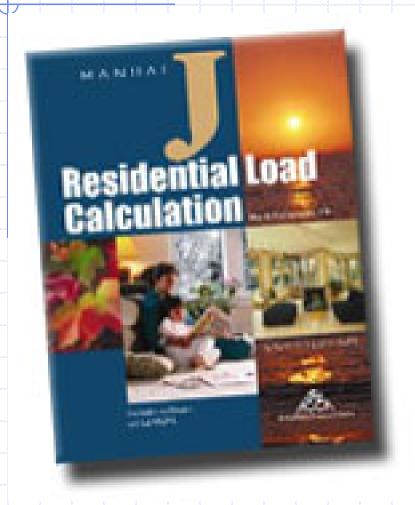
Residential Energy Services Network

Eighth Edition, ASHRAE 20 RESNET Fundamentals, or an equiv procedure, using the follow

Recognize This?

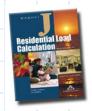


### ACCA Manual J v8



# The Standard in the Industry



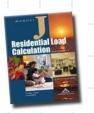


The heating and cooling load estimates affect every aspect of the system design procedure

- From system selection
- To equipment selection procedures
- To placement and selection of air distribution hardware
- To duct routing and airway sizing or pipe layout and sizing

Because of this the load calculation must be as accurate as possible

#### Value of Manual J



- Eliminate Under-sizing of Heating & Cooling Equipment
- Eliminate Over-sizing of Heating & Cooling Equipment
- Humidity Control During the Cooling Season
- Eliminate Comfort Problems

# Relating to Cooling Under Sizing Equipment

The obvious problem with undersized equipment is that it will not maintain the desired temperature. However, slightly undersized cooling equipment (by a margin of 10% or less) may actually provide more comfort at a lower cost.



# Oversized Equipment Causes

- short-cycles
- marginalized temperature control
- pockets of stagnate air
- degrades humidity control during the

cooling season

requires larger duct runs



# Oversized Equipment Causes

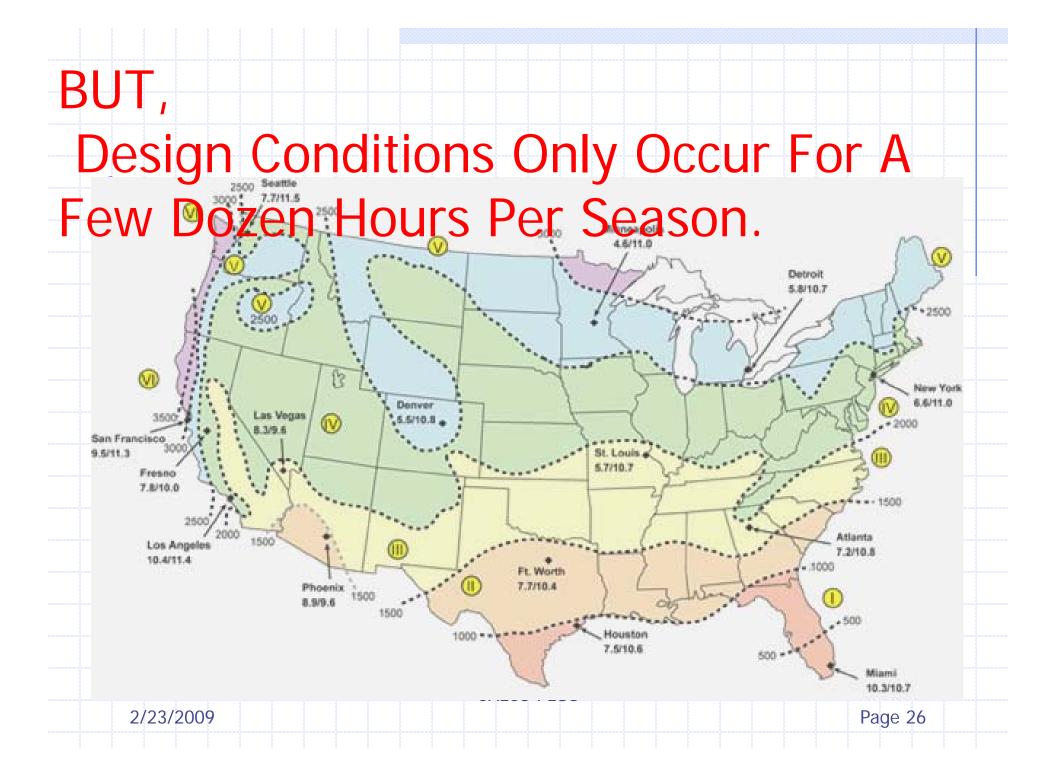
- increases the installed cost
- increases the operating cost
- increases the demand on our utilities
- adds unnecessary stress on equipment





# Humidity Control During The Cooling Season

- Sensible and latent cooling loads are imposed on buildings located in hot humid climates.
- When the summer design condition occurs, properly sized equipment will operate continuously or almost continuously, both loads will be neutralized, and the occupants will be comfortable.

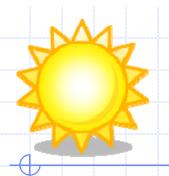


# **Design Conditions**

#### Table 1A

Outdoor Design Conditions For the United States and Canada

	Elevation	Latitude	Winter	Summer						
ocation	Feet	Degrees North	Heating 99% Dry Bulb	Cooling 1% Dry Bulb	Coincident Wet Bulb	Design Grains 55% RH	Design Grains 50% RH	Design Grains 45% RH	Daily Range (DR)	
St. Augustine	10	29	35	89	78	59	66	72	М	
St. Petersburg	11	28	47	93	79	59	66	72	М	
Sanford	55	28	38	93	76	39	46	52	М	
Sarasota/Bradenton	30	27	43	92	79	61	68	74	М	
Tallahassee AP	55	30	28	93	76	39	46	52	M	
Татра АР	19	28	40	91	77	49	56	62	М	
Valpariso, Eglin AFB	85	30	33	90	78	57	64	70	М	
Vero Beach	13	27	43	90	78	57	64	70	М	
West Palm Beach AP	15	26	47	90	78	57	64	70	М	



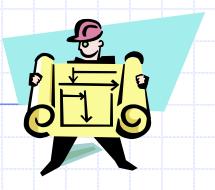


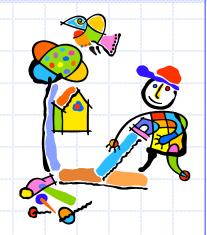


Outdoor design conditions used to estimate heating and cooling loads do not represent the most severe weather conditions experienced at a particular location.

However, they do represent extremes that, on average, will not be exceeded for more than a few dozen hours per season.

This means that when heating and cooling loads are based on Table 1, recommended design conditions, comfort and performance are optimized for thousand of hours per season.





Load estimating and equipment sizing concepts must be explained to the builders and home owners because they do not understand that installation and operating cost increase and long term comfort decreases when load estimates are based on record-setting weather conditions (MJ8, A3-2)



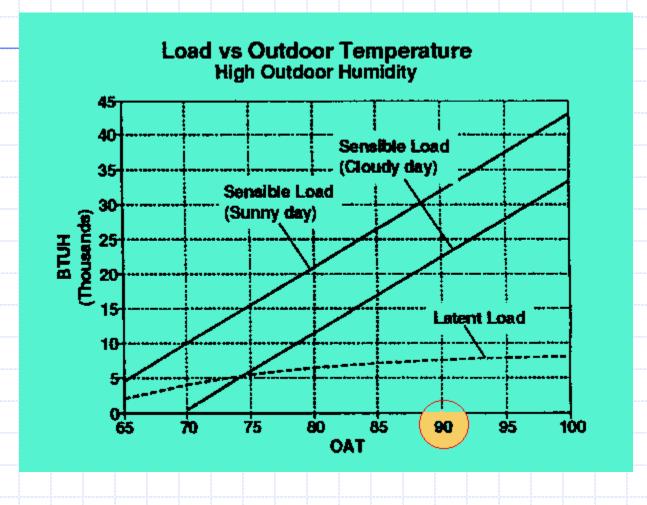


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2/23/2009

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Using Table 1 from ACCA Manual J for West Palm Beach the summer outdoor dry bulb temperature is 90°

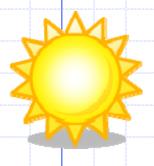


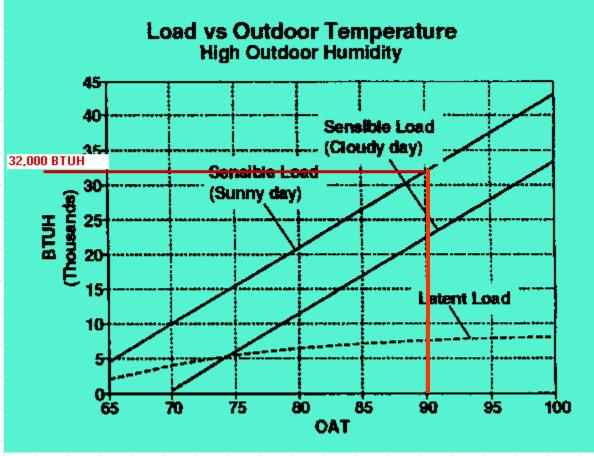
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2/23/2009

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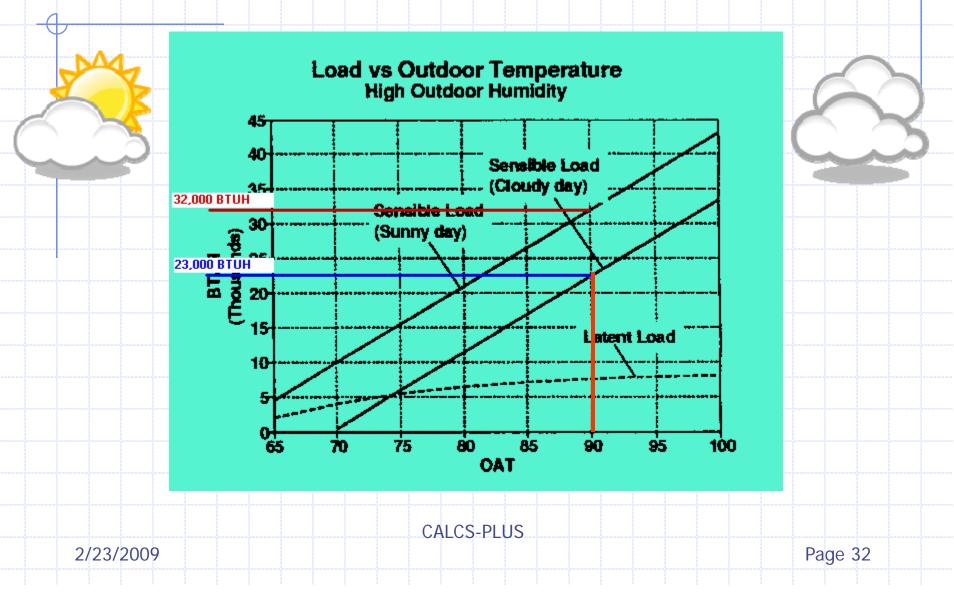
At peak load conditions, the HVAC load calculations shows the net gain on the building is 32,000 BTUH total.



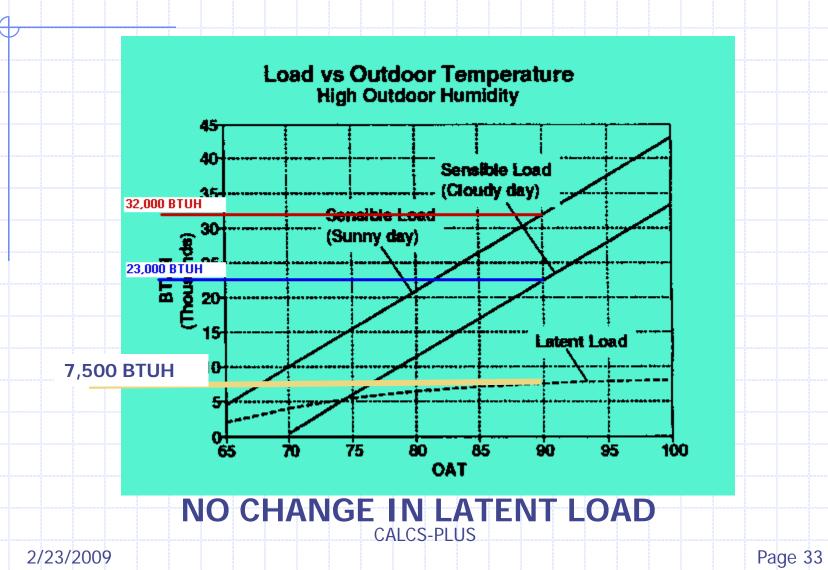




50% of the time our temperatures range is in the moderate temperature zone. The net gain could drop to 23,000 BTU/H on a 90° day if the sun is behind the clouds.

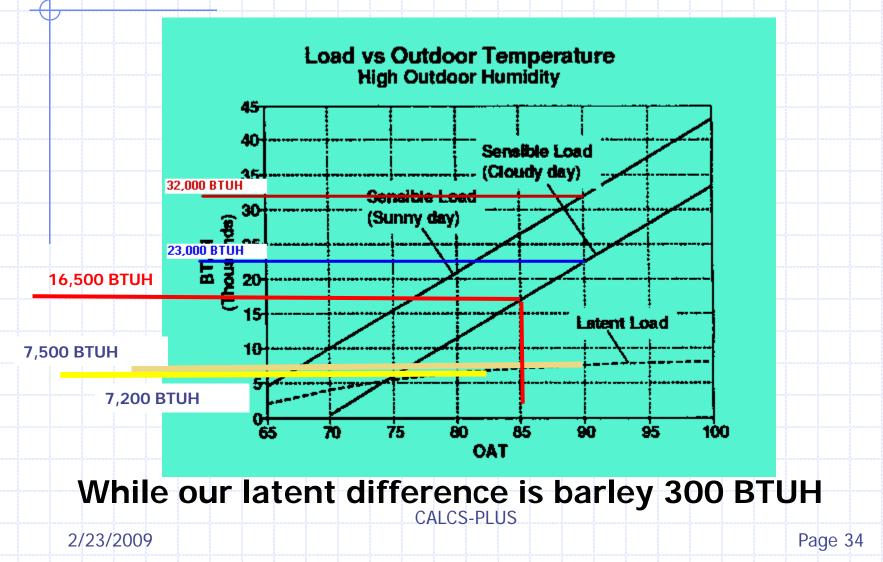


Sensible load variation shows a difference of 9000 BTUH while our latent load remains the same!

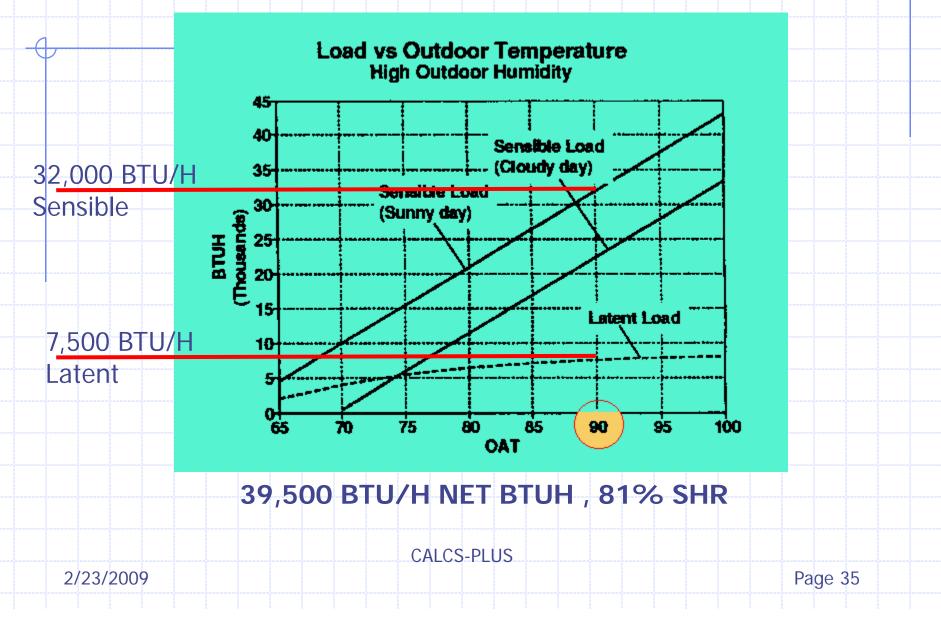


Lets say the temperature dropped to 85 when the sun went behind the clouds.

Sensible load drops to 16,500 BTU/H, a difference of 15,500 BTUH.



If your load calculation came out to 39,500 NET BTUH, what size system would you install?



#### MJ8 Sensitivities

Design conditions

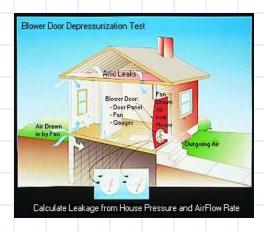
Building tightness

Fenestration

Air System Design & Installation



						anada			
Elevation   Feet	Latitude Degrees North	Winter Heating 99% Dry Bulb	Summer						
			Cooling 1% Dry Bulb	Coincident Wet Bulb	Design Grains 55% RH	Design Grains 50% RH	Design Grains 45% RH	Daily Range (DR)	
10	29	35	89	78	59	66	72	М	
11	28	47	93	79	59	66	72	М	
55	28	38	93	76	39	46	52	М	
30	27	43	92	79	61	68	74	М	
55	30	28	93	76	39	46	52	M	
19	28	40	91	77	49	56	62	М	
85	30	33	90	78	57	64	70	М	
13	27	43	90	78	57	64	70	М	
15	26	47	90	78	57	64	70	М	
	10 11 55 30 55 19 85 13	North  10 29 11 28 55 28 30 27 55 30 19 28 85 30 13 27	99% North Dry Bulb  10 29 35  11 28 47  55 28 38  30 27 43  55 30 28  19 28 40  85 30 33  13 27 43	North   Dry Bulb   Pry Bulb   P	North   Dry Bulb   D	Description   Description	Description   Description	Dog Bulb   Dry Bulb   Dry Bulb   Grains   Grains   Grains   S5% RH   S5%	





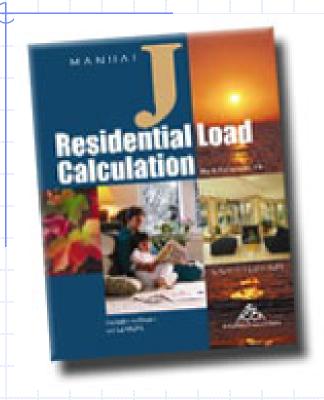
### Guidelines

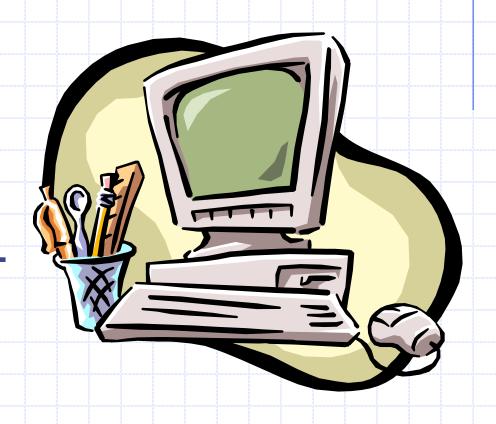
- Use outdoor design conditions recommended by Table 1 Manual J.
- Use the default indoor design conditions recommended by Manual J.
- Take full credit for all internal shading devices and external overhangs.
- Use internal shading devices that are compatible with the type of room.

## Guidelines

- Do not use internal shade if the room is specifically used for day lighting.
- Use the tested performance coefficients when known.
- Take full credit for all insulation & sealing efforts.
- Take full credit for insulated & sealed duct runs located in unconditioned space.

## ACCA Manual J v8





# A Computer Only Procedure

From "Addendum B" from ACCA Manual J®

Addendum B to

ACCA Manual J

#### Residential Load Calculation

Eighth Edition

ANSI/ACCA Man J 2-2004

ISBN# 1-892765-27-6

This addendum updates Version 1.10 of Manual J Eighth Edition (MJ8 $^{\text{MJ}}$ ) and addresses AED Protocol Revisions to the MJ8 $^{\text{MJ}}$  procedures.

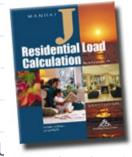
#### Executive Summary

Now that the industry and software houses have had time to work with the Eighth Edition of  $Manual J_{*}$ , ACCA has determined that AED simplifications would ease implementation by third-party software vendors and improve the understanding and use of MJ8 by practitioners. This addendum revises the adequate exposure diversity (AED) approach on window/glass exposures in the following manners:

- a) MJ8 shall become a computer-only procedure. (Note: A shorter, abridged version of MJ8 is under development that supports a hand calculation procedure aimed at single-family, detached dwellings with single-zone, constant-volume systems).
- A computer-only, hourly fenestration gain (HFG) procedure shall be used for all application scenarios.
- c) Calculations shall be made for midsummer, unless southerly-facing fenestration causes a peak gain in the fall.
- d) Hand calculation procedures for applications other than single family detached dwellings served by a single zone, constant volume system shall be abandoned in favor of computerized solutions.

# From Part of Section 1-16 ACCA Manual J 8<sup>th</sup> Edition

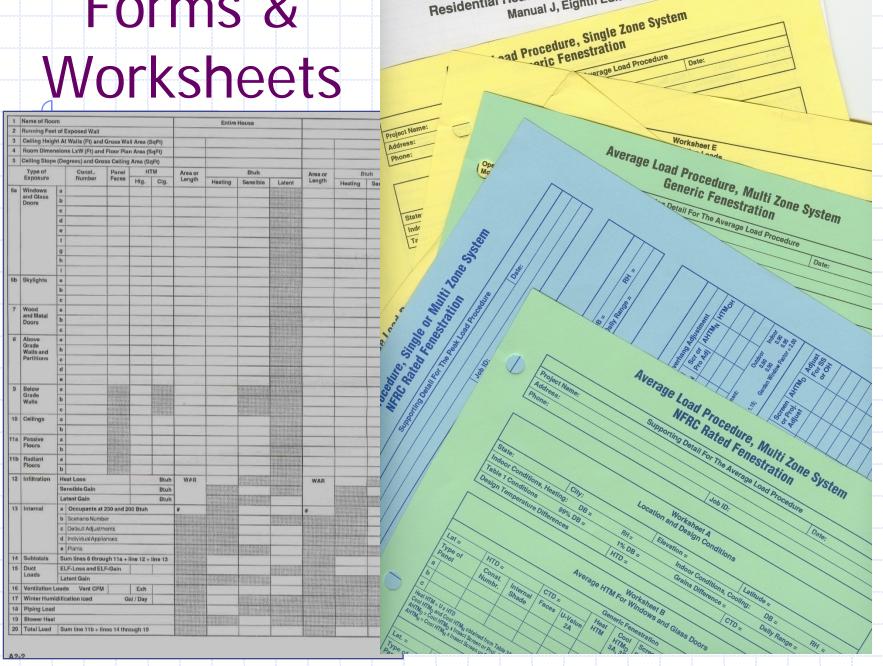
- Computerized method calculates load by month of year and time of day associated with each room load and with the equipment sizing load.
- Computer can generate solutions for 288 scenarios (12 month year and 24 hour day)





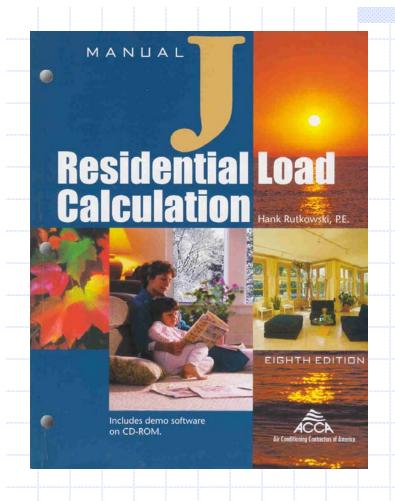


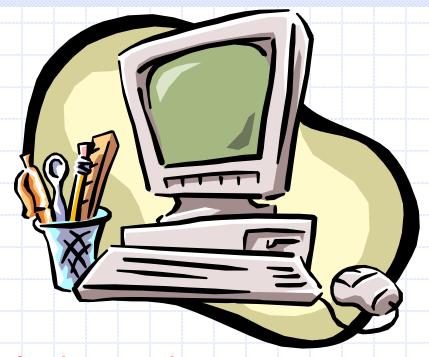
# Forms &



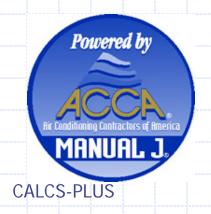
Residential Heat Loss and Heat Gain Estimate

Manual J, Eighth Edition





Only three software programs are recognized by ACCA as meeting the standards of Manual J residential load calculations.



Elite Software WrightSoft

Nitek

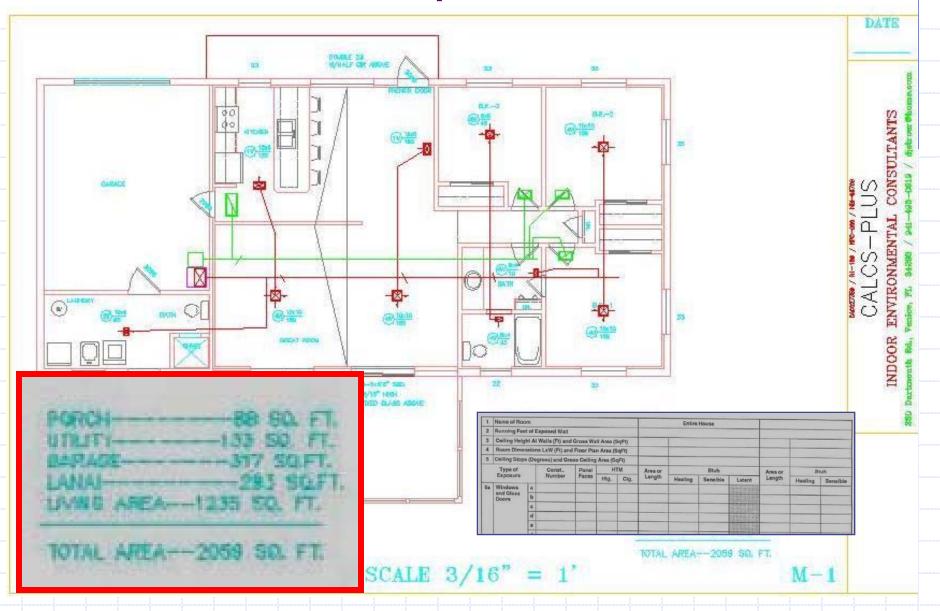
RHVAC

Right-J

**HVAC** Wizard



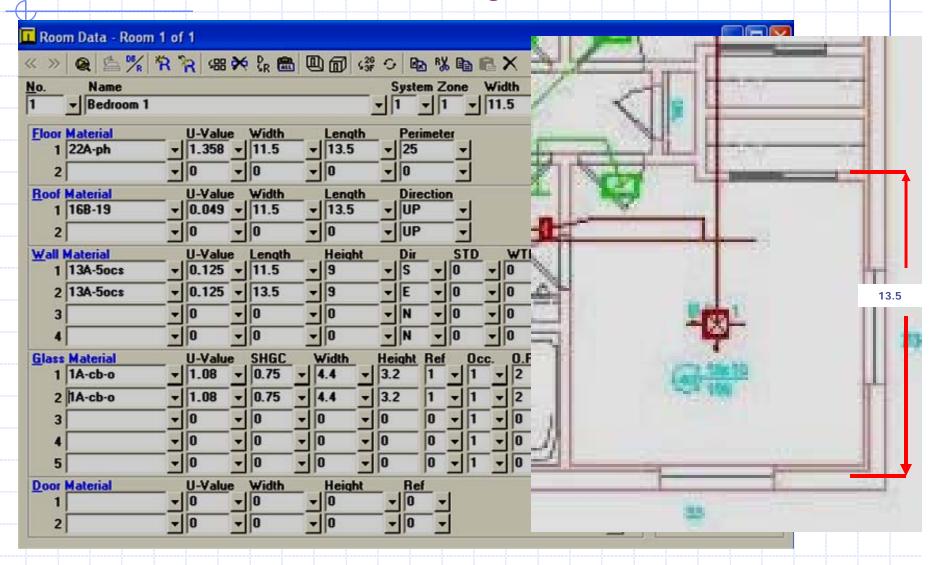
# Floor Plan Required.

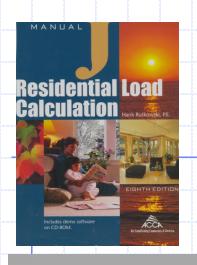


# Room x Room Entry

	Name of Roo						Entire	House									_				_			-
		of Exposed Wall																					_	-
		t At Walls (Ft) and																						-
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	Piping Load					411000		-						-	District of			TO SERVICE STREET	71110					
19	Blower Heat			E E					Article State Co.				10000	A CONTRACTOR OF THE PARTY OF TH	10000-07-09	100000	<b>FREE</b>		300		-	Tiberto.		
20	Total Load	Sum line 11b + li	nos 14 thr	ough 19					-			Name and Address of the Owner, where the Owner, which is the Owner							200000000000000000000000000000000000000	1		100000		
				_																				

# Room Entry Data





## Table 1A

RHVAC weather data base comes directly from ACCA Manual J version 8 Table 1A & 1B(micro climates).

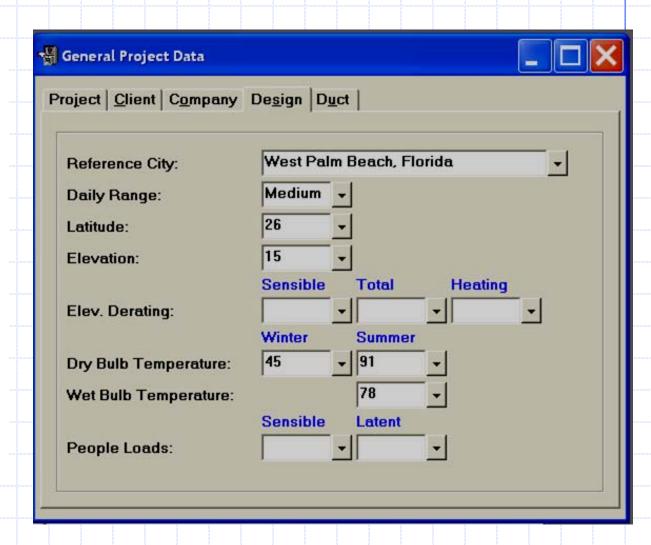
Table 1A
Outdoor Design Conditions For the United States and Canada

	Elevation	Latitude	Winter			Sum	mer		
ocation	Feet	Degrees North	Heating 99% Dry Bulb	Cooling 1% Dry Bulb	Coincident Wet Bulb	Design Grains 55% RH	Design Grains 50% RH	Design Grains 45% RH	Daily Range (DR)
St. Augustine	10	29	35	89	78	59	66	72	M
St. Petersburg	11	28	47	93	79	59	66	72	M
Sanford	55	28	38	93	76	39	46	52	M
Sarasota/Bradenton	30	27	43	92	79	61	68	74	M
Tallahassee AP	55	30	28	93	76	39	46	52	M
Tampa AP	19	28	40	91	77	49	56	62	M
Valpariso, Eglin AFB	85	30	33	90	78	57	64	70	M
Vero Beach	13	27	43	90	78	57	64	70	M
West Palm Beach AP	15	26	47	90	78	57	64	70	∘M:

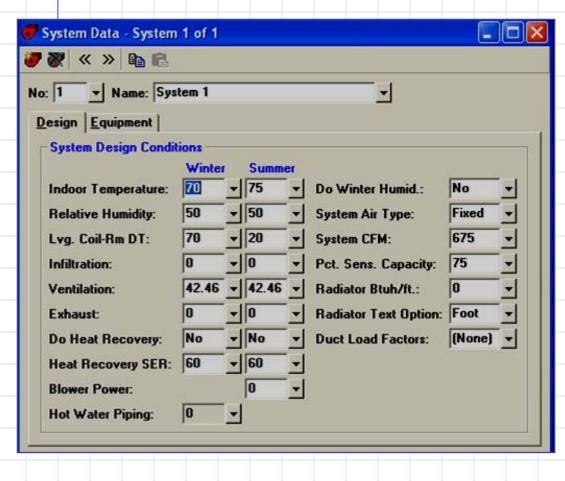
# Outdoor Design Conditions

The Data that is automatically filled in comes from Table 1A in ACCA Manual J 8<sup>th</sup> edition.

Outdoor Design Conditions For the United States and Canada.

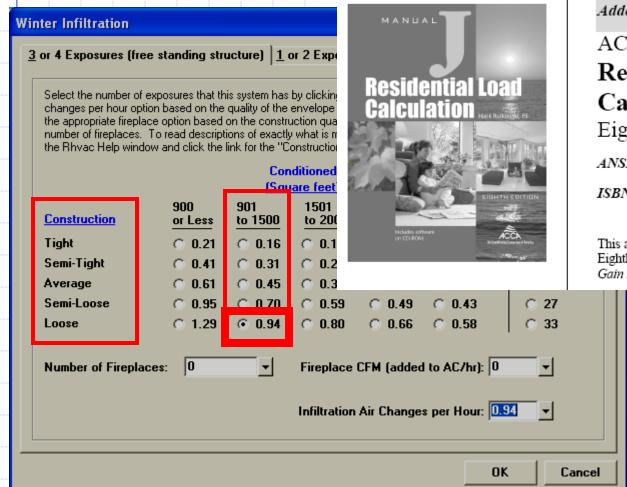


# System Information



- Indoor Design Conditions
- Infiltration
- Ventilation

# MJ8 & Infiltration For Winter



Addendum D to

ACCA Manual J<sub>®</sub>

#### Residential Load Calculation

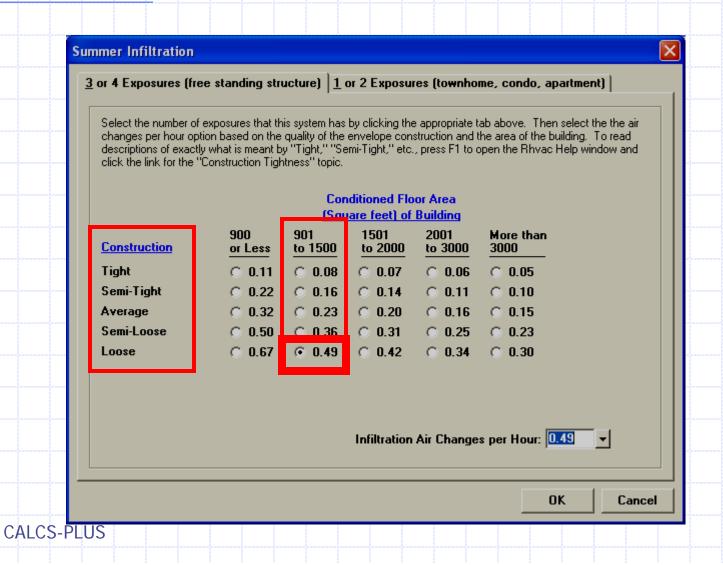
Eighth Edition

ANSI/ACCA Man J 2-2004

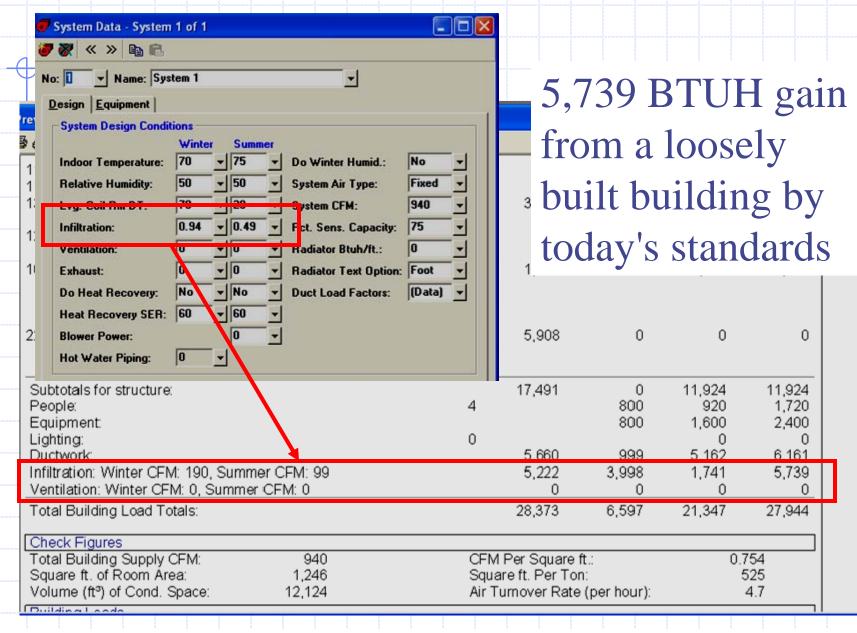
ISBN# 1-892765-27-6

This addendum updates Version 1.10 of Manual J Eighth Edition (MJ8<sup>TM</sup>) and addresses *Infiltration* Gain / Loss Revisions to the MJ8 procedures.

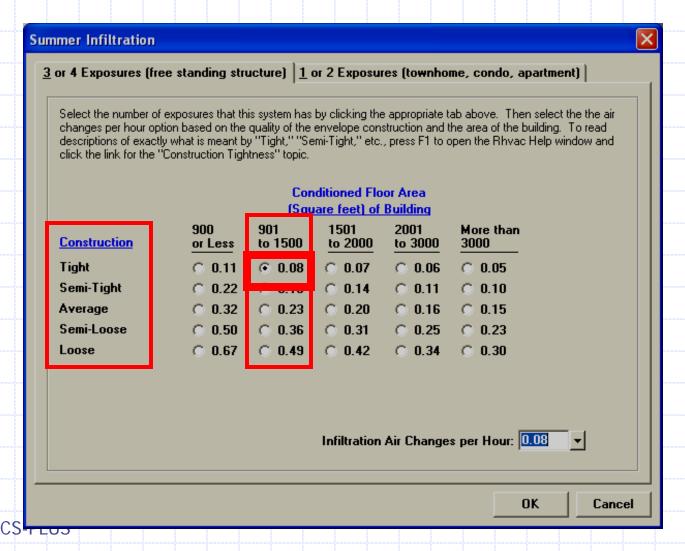
# MJ8 & Infiltration For Summer Loose Construction



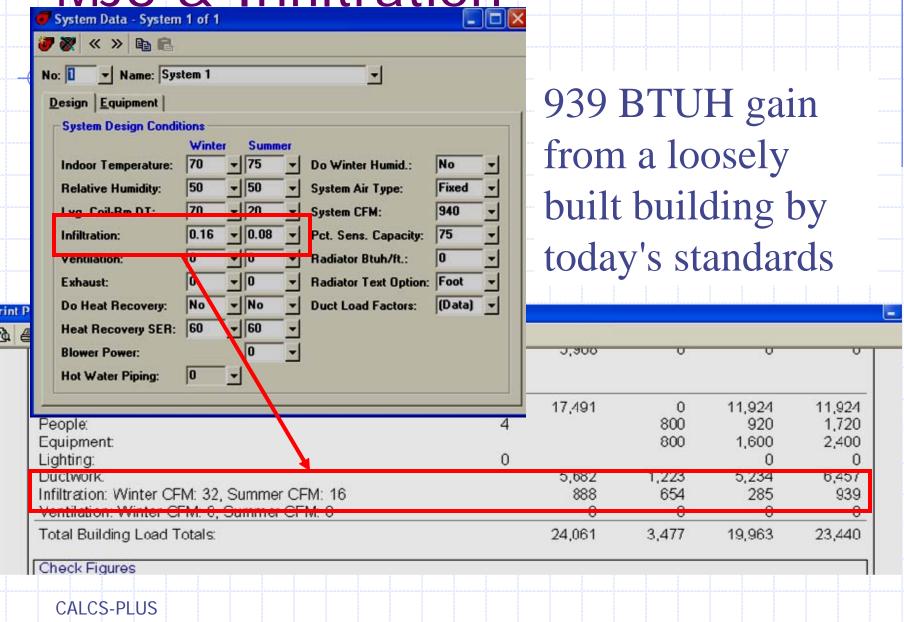
## MJ8 & Infiltration

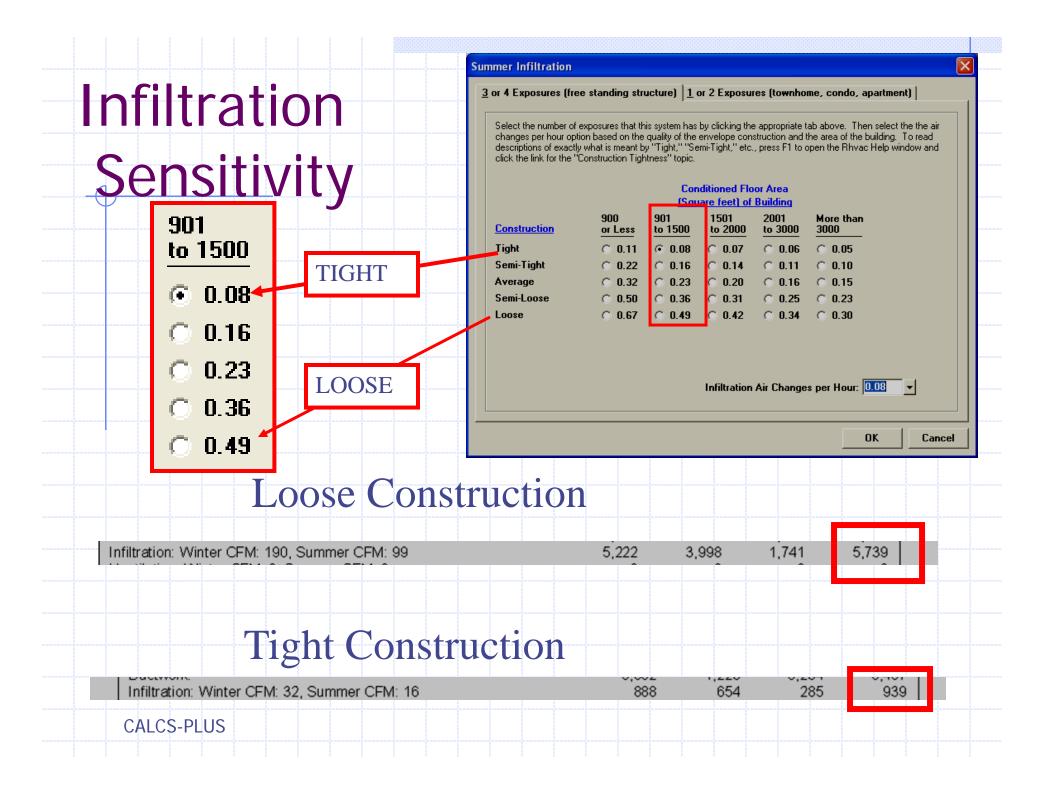


# MJ8 & Infiltration For Summer Tight Construction



MJ8 & Infiltration





# MJ8 & Duct Leakage



## MJ8 & Duct Design



Design room CFM (airflow)

## **Duct Loads**

Addendum C to

ACCA Manual J<sub>®</sub>

### Residential Load Calculation

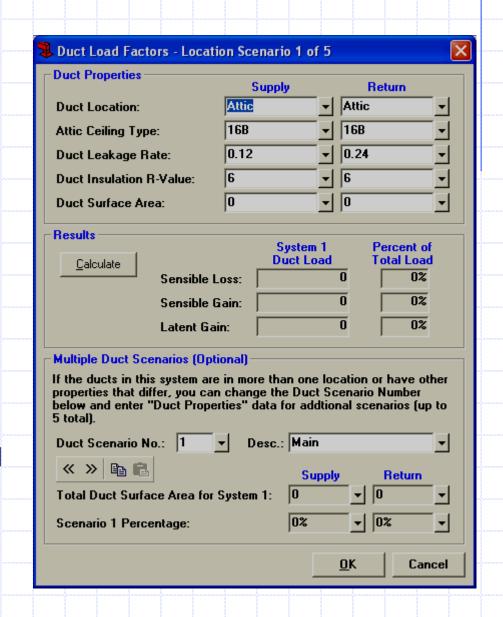
Eighth Edition

ANSI/ACCA Man J 2-2004

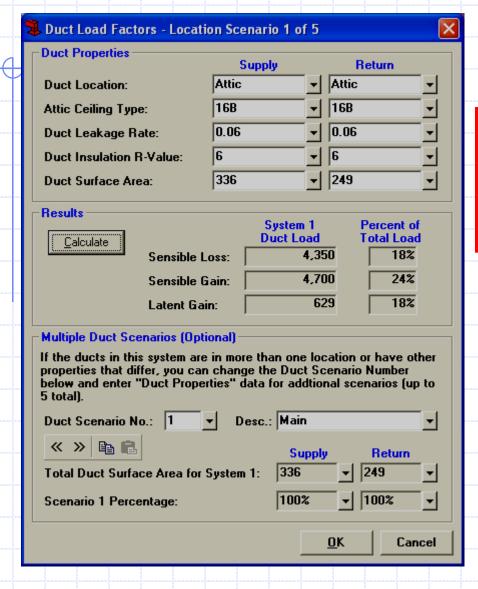
ISBN# 1-892765-27-6

This addendum updates Version 1.10 of Manual J Eighth Edition (MJ8<sup>™</sup>) and addresses *Duct Gain / Loss Revisions* to the MJ8 procedures.

Ducts located in the unconditioned space also have a heat gain that adds to the cooling load of the building.



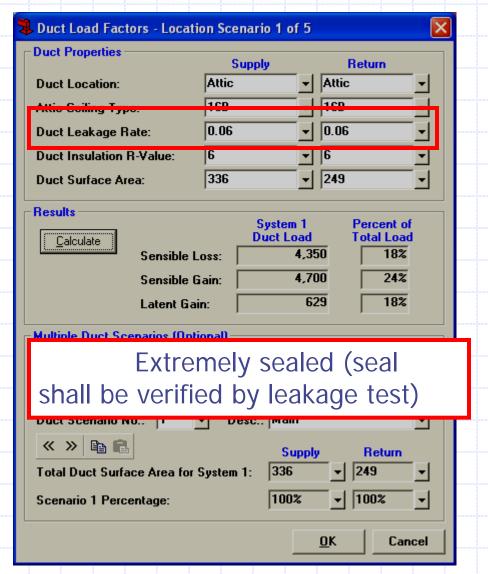
## Calculate Duct Loads

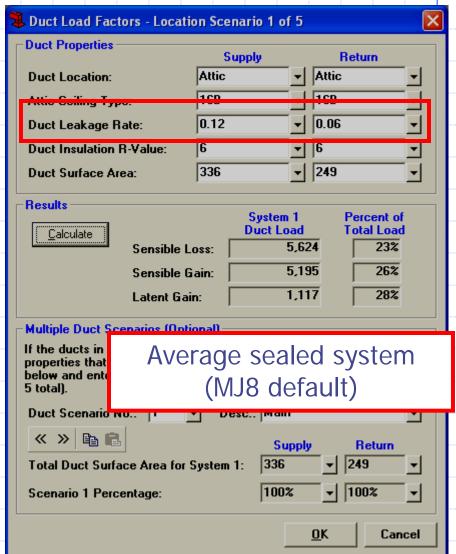


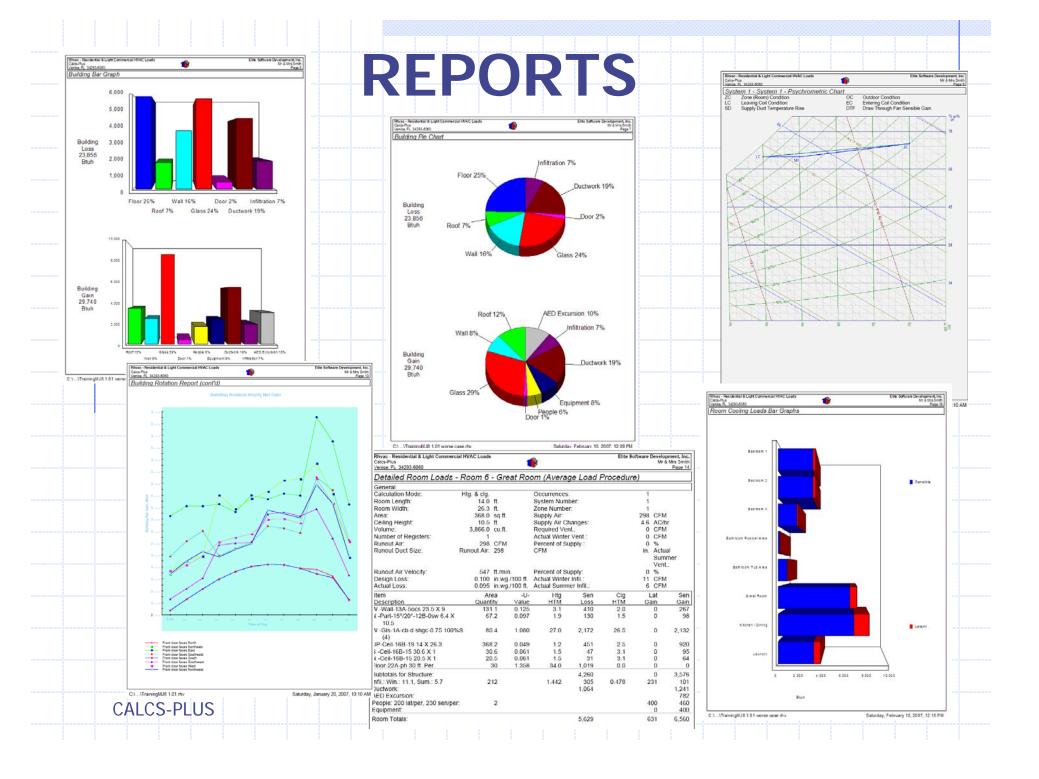
The Sensible Loss, Sensible Gain, and the Latent Gain are calculated for the duct system.



### What If?







### **Envelope Materials**

otal Building Summary Loads					
component	Area	Sen	Lat	Sen	Total
escription	Quan	Loss	Gain	Gain	Gain
A-cb-o: Glazing-Single pane, operable window, clear, metal frame with break, outdoor insect screen with 50% coverage, white or reflective color drapes with tight weave with 50% coverage, u-value 1.08	115.4	3,114	0	2,466	2,466
A-cb-d: Glazing-Single pane, sliding glass door, clear, metal frame with break, outdoor insect screen with 100% coverage, u-value 1.08	80.4	2,172	0	2,132	2,132
)A-b: Glazing-French door, single pane clear glass, metal frame with break, u-value 0.97	20.1	487	0	537	537
J: Door-Metal - Fiberglass Core	20.1	302	0	326	326
D: Door-Wood - Solid Core	20.1	157	0	118	118
A-5ocs: Wall-Block, board insulation only, R-5 board insulation, open core, siding finish	999.7	3,124	0	2,039	2,039
PB-0sw: Part-Frame, R-11 insulation in 2 x 4 stud cavity, no board insulation, siding finish, wood studs	308.1	597	0	448	448
6B-19: Roof/Ceiling-Under attic or knee wall, Vented Attic, No Radiant Barrier, Dark Asphalt Shingles or Dark Metal, Tar and Gravel or Membrane, R-19 insulation	1285.6	1,575	0	3,213	3,213
B-15: Roof/Ceiling-Under attic or knee wall, Vented Attic, No Radiant Barrier, Dark Asphalt Shingles or Dark Metal, Tar and Gravel or Membrane, R-15 insulation	84.8	130	0	264	264
A-ph-c: Floor-Slab on grade, No edge insulation, no insulation below floor, carpet covering, passive, heavy moist soil	174	5,908	0	0	0
uhtotale for etructure:		17 566	n	11 5/12	11 5/12

# Internal and Other Gains Check Figures

#### **Net Results**

Subtotals for structure:		17,566	0	11,543	11,543
People:	4		800	920	1,720
Equipment:			1,200	1,200	2,400
Lighting:	0			0	0
Ductwork:		4,510	647	4,818	5,465
Infiltration: Winter CFM: 65, Summer CFM: 33		1,780	1,350	588	1,938
Ventilation: Winter CFM: 0, Summer CFM: 0		0	0	0	0
Total Building Load Totals:		23,856	3,997	19,069	23,066

Check Figures

Total Building Supply CFM:	867	CFM Per Square ft.:	0.675
Square ft. of Room Area:	1,285	Square ft. Per Ton:	606
Volume (ft <sup>s</sup> ) of Cond. Space:	12,535	Air Turnover Rate (per hour):	4.2

**Building Loads** 

Total Heating Required With Outside Air:	23,856	Btuh	23.856 MBH
Total Sensible Gain:	19,069	Btuh	83 %
Total Latent Gain:	3,997	Btuh	17 %
Total Cooling Required With Outside Air:	23,066	Btuh	1.92 Tons (Based On Sensible + Latent)
			2.12 Tons (Based On 75% Sensible
			Capacity)

#### Notes

Calculations are based on 8th edition of ACCA Manual J.

All computed results are estimates as building use and weather may vary.

Be sure to select a unit that meets both sensible and latent loads.

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CALCS-PLUS

2/23/2009

## Room Loads

#### Rhvac - Residential & Light Commercial HVAC Loads

Elite Software Development, In College Station, TX 77845-4491



#### Elite Software Development, Inc.

Mr & Mrs Smith Page 4

#### Load Preview Report

Scope	Has AED	Net Ton	Rec Ton	ft² /Ton	Area	Sen Gain	Lat Gain	Net Gain	Sen Loss	Sys Htg CFM	Sys Clg CFM	Sys Act CFM	Duct Size
Buildin g		1.92	2.12	607	1,285	19,057	3,997	23,054	23,839	1,000	1,000	1,000	
System 1	Yes	1.92	2.12	607	1,285	19,057	3,997	23,054	23,839	1,000	1,000	1,000	0*
Diuct Latent							647	647					
Zone 1					9 17	14,414	2,719	17,133	18,231	765	676	676	
1-Bedroom 1					155	2,343	246	2,589	3,377	142	110	110	1-6
2-Bedroom 2					155	2,343	246	2,589	3,377	142	110	110	1-6
3-Bedroom 3					120	1,278	113	1,391	1,680	70	60	60	1-4
4-Bathroom Powder Area					48	156	0	156	73	3	7	7	1-4
5-Bathroom Tub Area					43	627	77	704	990	42	29	29	1-4
7-Kitchen / Dining					276	4,944	1,406	6,350	4,619	194	232	232	1-9
8-Laundry					120	2,724	631	3,355	4,115	173	128	128	1-7
Zone 2					368	6,904	631	7,535	5,608	235	324	324	
6-Great Room					368	6,904	631	7,535	5,608	235	324	324	1-10
Sum of room airflows may be greater than:	system airflow	becaus	e										
system has multiple zones.													

# Building Rotation Report

Rhvac - Residential & Light Commercial HVAC Loads Calcs-Plus Venice, FL 34293-6060



Elite Software Development, Inc. Mr & Mrs Smith Page 8

#### Building Rotation Report

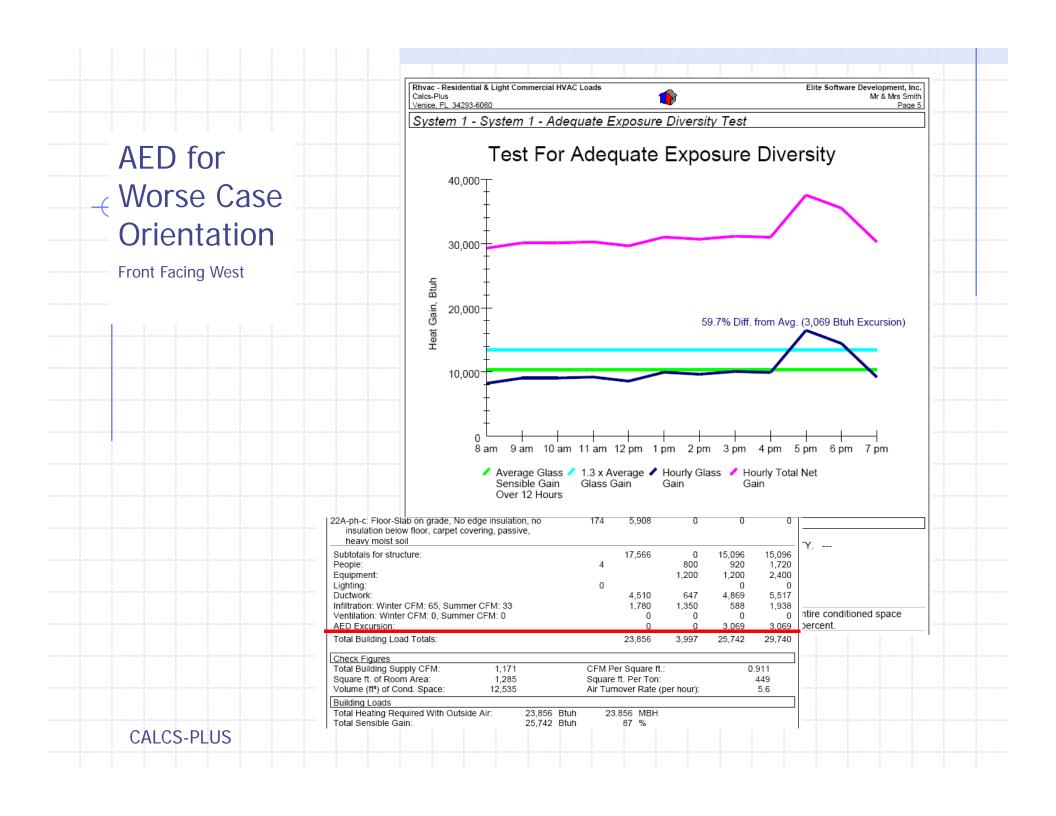
All rotation degree values in this report are clockwise with respect to the project's original orientation. Building orientation as entered (zero degrees rotation): Front door faces South

	Individual Rooms									
		0°	45°	90°	135°	180°	225°	270°	315°	High
	Rm. Room	Rot.	Duct							
	No. Name	CFM	Size							
^	System 1:									
	Zone 1:									
	1 Bedroom 1	91	104	*144	130	91	123	133	102	1-7
	2 Bedroom 2	91	134	*144	100	91	95	133	132	1-7
	3 Bedroom 3	51	72	*78	55	51	52	71	71	1-5
×	4 Bathroom Powder	7	8	*8	8	7	7	7	8	1-4
	Area									
۸.	5 Bathroom Tub Area	25	27	*36	34	25	32	34	26	1-4
	6 Great Room	276	296	298	*435	276	411	274	292	1-12
	7 Kitchen / Dining	204	290	*315	236	204	223	289	286	1-10
-	8 Laundry	122	133	*147	138	122	131	135	131	1-7

<sup>\*</sup> Indicates highest CFM of all rotations.

Rotation	Front door	Supply	Sensible	Latent	Net	Recommended
Degrees	Faces	CFM	Gain	Gain	Tons	Tons
0°	South	867	19,069	3,997	1.92	2.1
45°	Southwest	1,064	23,403	3,997	2.28	2.6
90°	West	*1,171	*25,742	3,997	*2.48	*2.8
135°	Northwest	1,136	24,981	3,997	2.41	2.7
180°	North	867	19,069	3,997	1.92	2.1
225°	Northeast	1,075	23,629	3,995	2.30	2.6
270°	East	1,075	23,631	3,995	2.30	2.6
315°	Southeast	1,050	23,081	*3,998	2.26	2.5

<sup>\*</sup> Indicates highest value of all rotations.



## Building Rotation Report

The Building Rotation Report calculates required cooling load for each of eight directions along with the required room CFM for each room.

This is very useful if the home does not have AED and it will be located in a subdivision and orientation is not known yet (worst-case direction).

Rhvac - Residential & Light Commercial HVAC Load Calcs-Plus Venice, FL 34293-6060



lite Software Development, Inc Mr & Mrs Smith

#### **Building Rotation Report**

All rotation degree values in this report are clockwise with respect to the project's original orientation. Building orientation as entered (zero degrees rotation): Front door faces South

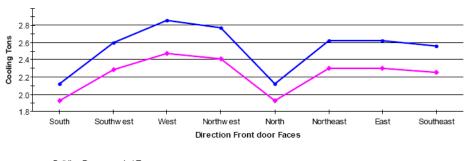
	Individual Rooms									
×	Day Dayer	0°	45°	90°	135°	180°	225°	270°	315°	High
	Rm. Room No. Name	Rot. CFM	Duct Size							
^	System 1:									~~
	Zone 1:									
	1 Bedroom 1	91	104	*144	130	91	123	133	102	1-7
	2 Bedroom 2	91	134	*144	100	91	95	133	132	1-7
	3 Bedroom 3	51	72	*78	55	51	52	71	71	1-5
	4 Bathroom Powder Area	7	8	*8	8	7	7	7	8	1-4
	<li>5 Bathroom Tub Area</li>	25	27	*36	34	25	32	34	26	1-4
	6 Great Room	276	296	298	*435	276	411	274	292	1-12 ~~
	7 Kitchen / Dining	204	290	*315	236	204	223	289	286	1-10
	8 Laundry	122	133	*147	138	122	131	135	131	1-7

<sup>\*</sup> Indicates highest CFM of all rotations.

Whole Buil	ding					50	
Rotation	Front door	Supply	Sensible	Latent	Net	Recommended	
Degrees	Faces	CFM	Gain	Gain	Tons	Tons	
0°	South	867	19,069	3,997	1.92	2.12	
45°	Southwest	1,064	23,403	3,997	2.28	2.60	
90°	West	*1,171	*25,742	3,997	*2.48	*2.86	
135°	Northwest	1,136	24,981	3,997	2.41	2.78	
180°	North	867	19,069	3,997	1.92	2.12	
225°	Northeast	1,075	23,629	3,995	2.30	2.63	
270°	East	1,075	23,631	3,995	2.30	2.63	
315°	Southeast	1,050	23,081	*3,998	2.26	2.56	

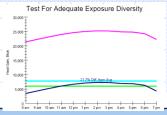
<sup>\*</sup> Indicates highest value of all rotations

#### **Building Rotation Tonnage**



Building Recommended Tonnage
Building Net Tonnage

# Our home has AED so the load does not change much from when rotated.

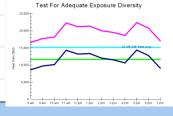


Whole Buil	aing					
Rotation	Front door	Supply	Sensible	Latent	Net	Recommended
Degrees	Faces	CFM	Gain	Gain	Tons	Tons
0°	South	867	19,069	3,997	1.92	2.12
45°	Southwest	1,064	23,403	3,997	2.28	2.60
90°	West	*1,171	*25,742	3,997	*2.48	*2.86
135°	Northwest	1,136	24,981	3,997	2.41	2.78
180°	North	867	19,069	3,997	1.92	2.12
225°	Northeast	1,075	23,629	3,995	2.30	2.63
270°	East	1,075	23,631	3,995	2.30	2.63
315°	Southeast	1,050	23,081	*3,998	2.26	2.56

<sup>\*</sup> Indicates highest value of all rotations.

Whole Building

### If the home does not have AED!



vvnole Bul	laing					100
Rotation	Front door	Supply	Sensible	Latent	Net	Recommended
Degrees	Faces	CFM	Gain	Gain	Tons	Tons
0°	West	612	14,225	*3,014	1.44	1.58
45°	Northwest	677	15,658	3,014	1.56	1.74
90°	North	518	12,168	3,014	1.27	1.35 ~
135°	Northeast	708	16,338	3,014	1.61	1.82
180°	East	812	18,623	3,014	1.80	2.07
225°	Southeast	*819	*18,782	3,014	*1.82	*2.09
270°	South	527	12,358	3,014	1.28	1.37
315°	Southwest	735	16,939	3,014	1.66	1.88
315	Southwest	735	16,939	3,014	1.00	ı

<sup>\*</sup> Indicates highest value of all rotations.

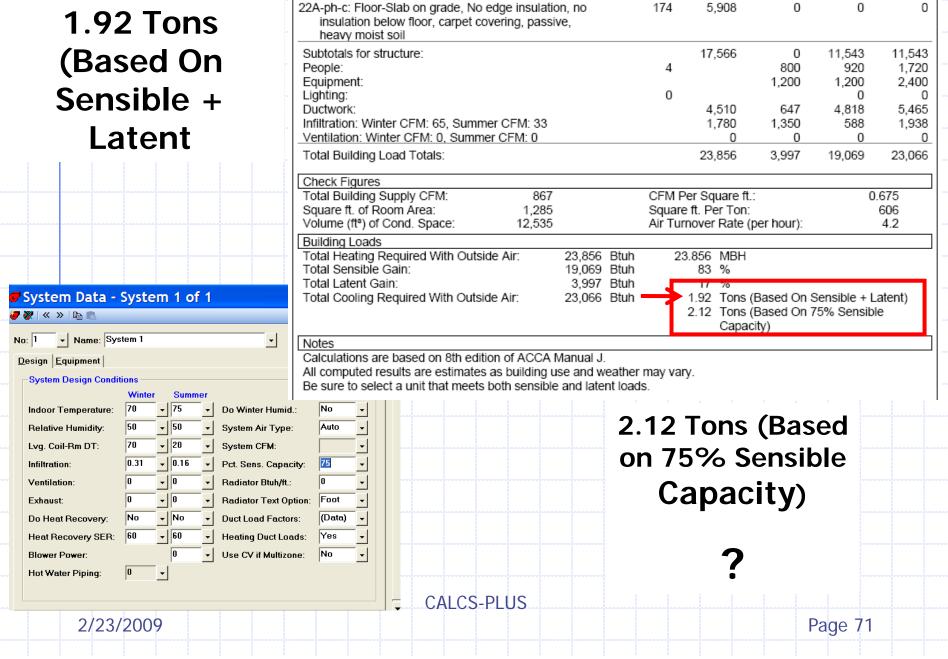
## **Equipment Selection**

Calos-Plus		4													
Venice, FL 34293-6080				•											
Total Building Summary Loads	4	0	1 -4	0											
Component Description	Area Quan	Sen Loss	Lat Gain	Sen Gain	Total Gain										
IA-cb-o: Glazing-Single pane, operable window, clear,	115.4	3,114	0	2,466	2,466										
metal frame with break, outdoor insect screen with		-,		2,	_,										
50% coverage, white or reflective color drapes with						TRANE RS		P	ERFOR	MANCE	DATA	COO	LING	F	ebruary 10, 200
tight weave with 50% coverage, u-value 1.08		0.470		0.400	0.400					U.S. (EN	GLISH)				
A-cb-d: Glazing-Single pane, sliding glass door, clear,	80.4	2,172	0	2,132	2,132			(Cap	acities are n	et in btuh/10	000 - indo	or fan he	at deducted)		
metal frame with break, outdoor insect screen with 100% coverage, u-value 1.08						0.41									
0A-b: Glazing-French door, single pane clear glass,	20.1	487	0	537	537	Outdoor M 2TTR 3030						or Mod			
metal frame with break, u-value 0.97	20.1	401		001	00,	Z1 1 K 3U3	UAI				IWI	CUSIE	13		
4 l. Dana Matal. Filancian Con-	M - 1		•	4.1.	- 8/4	IO D			11.	1					
1D: Door-Wood - Solid Core	viai	ch	ına	Th	e IVI	J8 Re	26	Ш	ITS	TO					
	VICE		'' '9			30 110							ction Fac	etors - Ot	her Airflows
insulation, open core, siding finish 2B-0sw; Part-Frame, R-11 insulation in 2 x				_										875	1125
no board insulation, siding finish, wood s	nut	act	Tir	r/c	: PA	rform	าว	n	CO		at	2			And a second
6B-19: Roof/Ceiling-Under attic or knee wa	IIGI	act	.ui v	GI 3			I		CC		at	a	apacity	0.98	1.02
Attic, No Radiant Barrier, Dark Asphalt Sg.co or						Indoor Fan Pov	war	= 23	6 wat	**		Compr	e Capacity ressor Kw	0.94	1.06 1.01
Dark Metal, Tar and Gravel or Membrane, R-19						Outdoor Fan P		= 15				Compi	lessor Aw	0.57	1.01
insulation	84.8	130	0	264	264	S.E.E.R		= 14	.00						
6B-15: Roof/Ceiling-Under attic or knee wall, Vented Attic, No Radiant Barrier, Dark Asphalt Shingles or	04.0	130	U	264	264										
Dark Metal, Tar and Gravel or Membrane, R-15															
insulation					_	Rated with 2	5 feet	of 3/4	suction and	5/16 li	quid lines	Ľ.			
2A-ph-c: Floor-Slab on grade, No edge insulation, no	174	5,908	0	0	0										
insulation below floor, carpet covering, passive,															
heavy moist soil					~		O.D.	I.D.	TOTAL	SENSI	BLE C	APACI	TY S	YSTEM	
Subtotals for structure:		17,566	0	11,543	11,543		D.B	W.B.	CAP	72	75	78	80	KW	
People: Equipment:	4		800 1,200	920 1.200	1,720 2,400		85	59	26.0				26.0	2.11	
Equipment. Lighting:	0		1,200	1,200	2,400		85	63	27.1	17.3	20.0	22.6	24.3	2.12	
Ductwork:	Ü	4.510	647	4.818	5.465		85	67	29.2				20.7	2.16	
nfiltration: Winter CFM: 65, Summer CFM: 33		1,780	1,350	588	1,938		95	59	24.7				24.7	2.30	
/entilation: Winter CFM: 0, Summer CFM: 0		0	0	0	0		95 95	63	25.7 27.7				23.8	2.31	
Total Building Load Totals:		23,856	3,997	19,069	23,066		105	63	24.3				23.2	2.51	
Ohaali Firmaa					°		105	67	26.2	12.6	15.2	17.8	19.6	2.55	
Check Figures Total Building Supply CFM: 867	CEM D	er Square ft		0	.675		105	71	28.3				15.9	2.57	
Square ft. of Room Area: 1,285		ft. Per Ton:			606		115	63	23.0		11100000		22.7	2.70	
Volume (ft <sup>s</sup> ) of Cond. Space: 12,535		nover Rate (			4.2		115 115	67 71	24.7				19.0 15.4	2.75	
Building Loads			. ,				112	/1	20.7	0.4	11.0	13.0	13.4	2.11	
Total Heating Required With Outside Air: 23,856 Bt	tuh 23	3.856 MBH					95	63	25.7	I.D.D.B =	75	19	9.4	2.31	
Total Sensible Gain: 19,069 Bt		83 %													
Total Latent Gain: 3,997 Bt		17 %	(D 0	0:											
Total Cooling Required With Outside Air: 23,066 Bt				Sensible + L 75% Sensibl											
		2.12 Tons Capa		10% SeriSiDi	IC III										
Notes		Оцра	J. 1,				a at sale	atad da-	gn condition						
Calculations are based on 8th edition of ACCA Manual J.						nanc	e at sele	cied dési	gn condition	15					
All computed results are estimates as building use and weat	ther may van	y.				* Dry coil cond	ition (To	tal Capa	city = Sensi	ble Capacity	)				
Be sure to select a unit that meets both sensible and latent I					_	T		17.17							
					3	Total capacity,	compress	sor KW	vand only fo	r wetcoil					
				CVI	CS-PL	All temperature	s in Degr	ree °F							TRAN
					LUJ-FL										

2/23/2009







16B-15: Roof/Ceiling-Under attic or knee wall, Vented

insulation

Attic, No Radiant Barrier, Dark Asphalt Shingles or Dark Metal, Tar and Gravel or Membrane, R-15

84.8

130

264

264

Check Figures   Total Building Supply CFM: 867   CFM Per Square ft.: Square ft. of Room Area: 1,285   Square ft. Per Ton: Volume (ft*) of Cond. Space: 12,535   Air Turnover Rate (per hour):	Total Building Load Totals:				23	,856	3,997
Square ft. of Room Área: 1,285 Volume (ft®) of Cond. Space: 12,535  Building Loads Total Heating Required With Outside Air: 23,856 Total Sensible Gain: 19,069 Btuh 83 % Total Latent Gain: 3,997 Btuh 17 %	Check Figures						
Volume (fts) of Cond. Space: 12,535 Air Turnover Rate (per hour):  Building Loads Total Heating Required With Outside Air: 23,856 Btuh 23.856 MBH Total Sensible Gain: 19,069 Btuh 83 % Total Latent Gain: 3,997 Btuh 17 %	Total Building Supply CFM:	867			CFM Per Sq	uare ft.:	
Building Loads Total Heating Required With Outside Air: 23,856 Btuh 23.856 MBH Total Sensible Gain: 19,069 Btuh 83 % Total Latent Gain: 3,997 Btuh 17 %	Square ft. of Room Area:	1,285			Square ft. Pe	er Ton:	
Total Heating Required With Outside Air: 23,856 Btuh 23.856 MBH Total Sensible Gain: 19,069 Btuh 83 % Total Latent Gain: 3,997 Btuh 17 %	Volume (ft <sup>s</sup> ) of Cond. Space:	12,535			Air Turnover	Rate (p	er hour):
Total Sensible Gain: 19,069 Btuh 83 % Total Latent Gain: 3,997 Btuh 17 %	Building Loads						
Total Latent Gain: 3,997 Btuh 17 %	Total Heating Required With Ou	tside Air:	23,856	Btuh	23.856	MBH	
-,	Total Sensible Gain:		19,069	Btuh	83	%	
	Total Latent Gain:		3,997	Btuh	17	%	
Total Cooling Required With Outside Air: 23,066 Btuh 1.92 Tons (Based On Ser	Total Cooling Required With Ou	tside Air:	23,066	Btuh	1.92	Tons (	Based On Ser
2.12 Tons (Based On 75%					2.12	Tons (	Based On 759
Capacity)						Capaci	ity)
Notes	Notes						
Calculations are based on 8th edition of ACCA Manual J.	Calculations are based on 8th e	dition of ACCA N	√lanual J				
All computed results are estimates as building use and weather may vary.	All computed results are estimate	ies as building u	se and w	eather	may vary.		

Be sure to select a unit that meets both sensible and latent loads.

Manufacturers performance cooling data (like the one at the right) will give system performance at conditions other than ARI

For the area of the country this home is going to be located we will be interested in how the system will perform at or near MJ8 design conditions of 91°F outdoor and 75°F @ 50% RH.

TRANE RS

#### ERFORMANCE DATA COOLING

ebruary 10, 2007

-- U.S. (ENGLISH) --

(Capacities are net in b tuh/1000 - indoor fan heat deducted)

Outdoor Model 2TTR3030A1 Indoor Model TWE031E13

Airflow = 1000

Values At ARI I	Ratin	g Cond	itions
Total Net Capacity	=	27800	Btuh
Airflow	=	1020	CFM
Compressor Power	=	1970	watts
Indoor Fan Power	=	236	watts
Outdoor Fan Power	=	150	watts
S.E.E.R	=	14.00	

Correction Fac	tors - O	ther Airflows
Airflow	875	1125
Total Capacity	0.98	1.02
Sensible Capacity	0.94	1.06
Compressor Kw	0.99	1.01

Rated with 25 feet of 3/4 suction and 5/16 liquid lines.

O.D.	I.D.	TOTAL	SENS	IBLE	CAPAC	CITY	SYSTEM
D.B	W.B.	CAP	72	75	78	80	KW
85	59	26.0	21.3	23.9	26.0	26.0	2.11
85	63	27.1	17.3	20.0	22.6	24.3	2.12
85	67	29.2	15.4	15.4	18.9	20.7	2.16
95	59	24.7	20.7	23.4	24.7	24.7	2.30
95	63	25.7	16.7	19.4	22.0	23.8	2.31
95	67	27.7	13.1	15.8	18.4	20.1	2.35
105	63	24.3	16.2	18.8	21.4	23.2	2.51
105	67	26.2	12.6	15.2	17.8	19.6	2.55
105	71	28.3	8.9	11.6	14.2	15.9	2.57
115	63	23.0	15.7	18.3	20.9	22.7	2.70
115	67	24.7	12.0	14.7	17.3	19.0	2.75
115	71	26.7	8.4	11.0	13.6	15.4	2.77
95	63	25.7	I.D.D.B =	75		19.4	2.31

Total capacity, compressor KW valid only for wetcoil

All temperatures in Degree oF



<sup>\*\*\*</sup> Performance at selected design conditions

<sup>\*</sup> Dry coil condition (Total Capacity = Sensible Capacity)

Total Net Capacity = 27800Btuh Airflow 1020 CFM Compressor Power 1970 watts Indoor Fan Power 236 watts Outdoor Fan Power 150 watts S.E.E.R 14 00

····	O.D.	I.D.	TOTAL	SENS	SIBLE (	CAPA	CITY	SYSTEM	
	D.B	<u>W.B.</u>	CAP	72	<u>75</u>	<u>78</u>	80	KW	
	8.5	59	26.0	21.3	23.9	26.0	26.0	2.11	
	8.5	63	27.1	17.3	20.0	22.6	24.3	2.12	
	8.5	67	29.2	15.4	15.4	18.9	20.7	2.16	
	95	59	24.7	20.7	23.4	24.7	24.7	2.30	
	95	63	25.7	16.7	19.4	22.0	23.8	2.31	
	95	67	21.1	13.1	10.8	18.4	20.1	2.35	
	105	63	24.3	16.2	18.8	21.4	23.2	2.51	
	105	67	26.2	12.6	15.2	17.8	19.6	2.55	
	105	71	28.3	8.9	11.6	14.2	15.9	2.57	
	115	63	23.0	15.7	18.3	20.9	22.7	2.70	
	115	67	24.7	12.0	14.7	17.3	19.0	2.75	
	<u>115</u>	71	<u>26.7</u>	8.4	11.0	<u>13.6</u>	<u>15.4</u>	<u>2.77</u>	
	95	63	25.7	I.D.D.B	= 75		19.4	2.31	
				CALCS-	PLU5				
2/23/2009								Page 73	

# MJ8 & the Energy Rater

The information you gather to do a energy rating is the same as required for an HVAC Load Calculation.

Do it to set yourself apart from your competition.

Do it to become a better Energy Rater.

Do it to provide another avenue for income.

## Larger Customer Base

AC Contractors know or at least had to have learned load calculations if they carry a licenses or certification.

AC contractors are busy running a company and don't have time to do room x room calculations.

If they were provided room x room calculations they would use them as a design tool.

# Diagnostic Tool

Start every diagnostic investigation with a room x room HVAC load calculation.

You will understand the construction of the building much better.

You will have a better understanding of the results of all the data gathered.

# A Plug for MJ8

The possibility for experiencing comfort problems at part load conditions can be minimized by observing the guidelines set forth in Manual J.

The Manual J calculation should take full advantage of legitimate opportunities to minimize the size of the estimated loads.

# Thank You

Questions?

